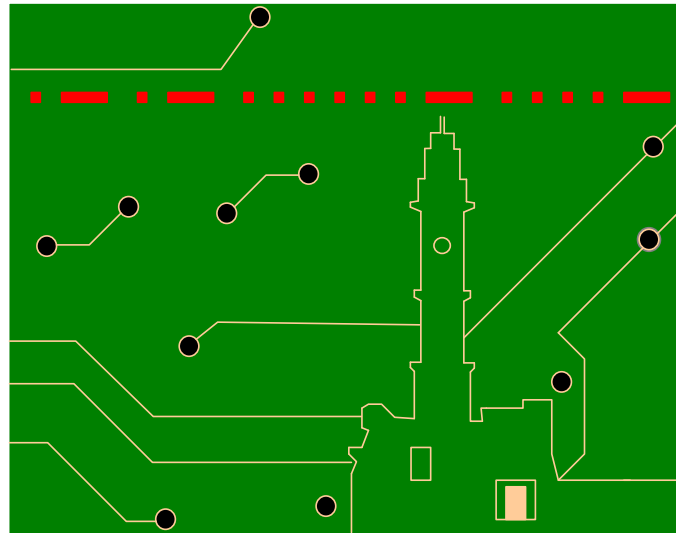


ΤΗΛ412 Ανάλυση & Σχεδίαση (Σύνθεση) Τηλεπικοινωνιακών Διατάξεων

Διάλεξη 3



Άγγελος Μπλέτσας

ΗΜΜΥ Πολυτεχνείου Κρήτης, Φθινόπωρο 2014

Lecture 3 – Basic Concepts (cont'd)

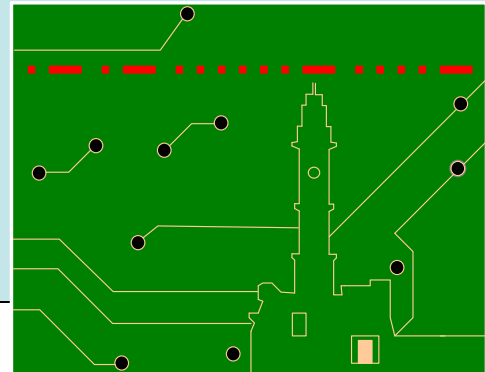
Basic Unknown Concepts:

- Previous lecture: Introduction to nonlinearities

(1-dB CP, IP3)

Today:

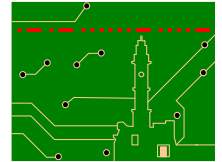
- Thermal noise of a resistor
- Calculating Noise Figure (NF)
- Notion of Sensitivity
- Notion of Dynamic Range



Διάλεξη 3

Most Figures for today's lecture come from:
B. Razavi, RF Microelectronics, Prentice Hall
1998.





Thermal noise voltage of a resistor

Assume resistor R , then thermal noise induced voltage across the resistor:

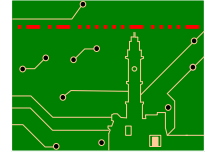
$$\overline{V_n^2} = 4 k T R = \text{average squared voltage for unit bandwidth (V}^2/\text{Hz)}$$

$k = 1.38 \times 10^{-23}$ Joules/K (Boltzmann constant)

T = absolute temperature (in Kelvin)

- Remark 1: stems from $\text{PSD} = 2 k T R$ of two-sided thermal noise which can be considered WHITE up to $|f| < 100$ GHz
- Remark 2: factor of 2 in voltage-squared above stems for considering both positive as well as negative freqs!
- Caution: PSD has units of power per unit bandwidth (Watt/Hz) but $\overline{V_n^2}$ has units of V^2/Hz [try $\text{BW} = 100\text{MHz}$, $R = 1\text{M}\Omega$ and test oscilloscope]

Remember Noise Figure?



$$\text{noise figure} = \frac{SNR_{\text{in}}}{SNR_{\text{out}}}$$

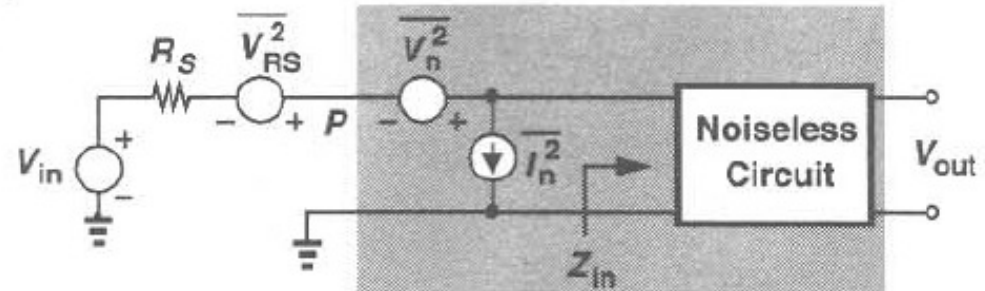
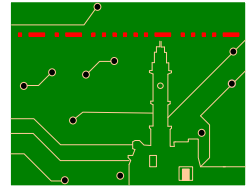
- Noiseless system (ideal) \Rightarrow NF = 1 (0 dB).
- Noise Figure of Cascaded Systems (Friis eq.):

$$NF_{\text{tot}} = 1 + (NF_1 - 1) + \frac{NF_2 - 1}{A_{p1}} + \dots + \frac{NF_m - 1}{A_{p1} \cdot \dots \cdot A_{p(m-1)}}$$

- NF of a stage decreases with gain of previous stage \Rightarrow
- ...initial stages are the most (NF)-critical!

Power gain
(not voltage
gain)

How do we calculate Noise Figure?



- Basic principle: we refer SNRs to input source resistance R_S .
 ...assuming VOLTAGE gain α from V_{in} to P
 and A_v from P to V_{out}

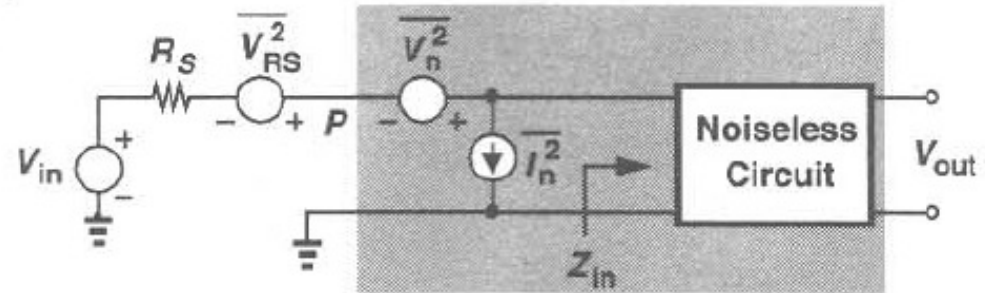
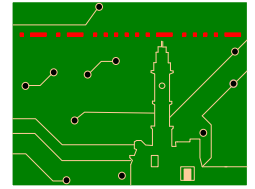
$$SNR_{in} = \frac{\alpha^2 V_{in}^2}{\alpha^2 V_{RS}^2}$$

$$SNR_{out} = \frac{\alpha^2 A_v^2 V_{in}^2}{[V_{RS}^2 + (V_n + I_n R_S)^2] \alpha^2 A_v^2}$$

$$= \frac{V_{in}^2}{[V_{RS}^2 + (V_n + I_n R_S)^2]}$$

Refer internal noise
at the device input!

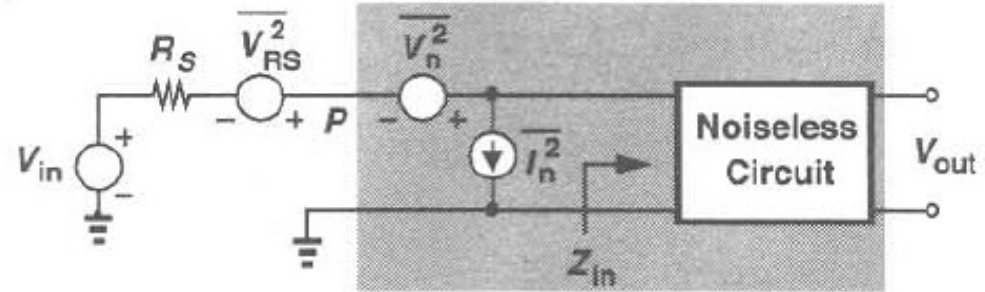
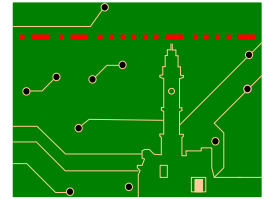
How do we calculate Noise Figure?



- Basic principle: we refer SNRs to input source resistance R_S .
 ...assuming VOLTAGE gain α from V_{in} to P
 and A_v from P to V_{out}

$$\begin{aligned} \text{noise figure} &= \frac{SNR_{in}}{SNR_{out}} = \frac{\overline{V_{RS}^2} + \overline{(V_n + I_n R_S)^2}}{\overline{V_{RS}^2}} \\ &= 1 + \frac{\overline{(V_n + I_n R_S)^2}}{\overline{V_{RS}^2}} \quad \Rightarrow \quad \text{(Per unit bandwidth)} \\ NF &= 1 + \frac{\overline{(V_n + I_n R_S)^2}}{4kTR_S} \end{aligned}$$

How do we calculate Noise Figure?



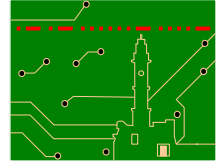
$$NF = 1 + \frac{\overline{(V_n + I_n R_S)^2}}{4kTR_S} \Rightarrow$$

$$A = aA_v$$

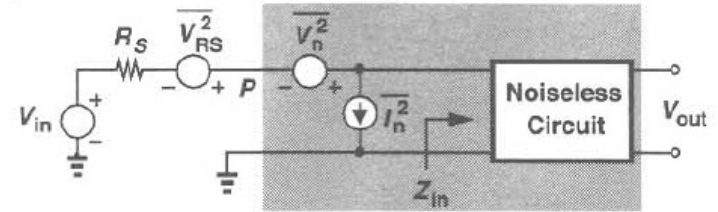
$$\begin{aligned} NF &= \frac{4kTR_S + \overline{(V_n + I_n R_S)^2}}{4kTR_S} \\ &= \frac{A^2 [4kTR_S + \overline{(V_n + I_n R_S)^2}]}{A^2} \frac{1}{4kTR_S} \\ &= \frac{V_{n,out}^2}{A^2} \frac{1}{4kTR_S}, \end{aligned}$$

Total measured noise at device output

How do we calculate Noise Figure?



$$\begin{aligned} NF &= \frac{4kTR_S + \overline{(V_n + I_n R_S)^2}}{4kTR_S} \\ &= \frac{A^2 [4kTR_S + \overline{(V_n + I_n R_S)^2}]}{A^2} \frac{1}{4kTR_S} \\ &= \frac{V_{n,out}^2}{A^2} \frac{1}{4kTR_S} \end{aligned}$$



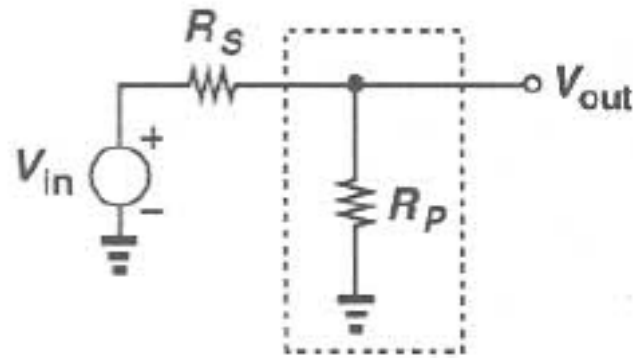
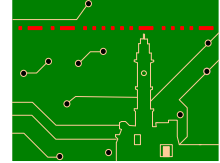
$$A = aA_v$$

- Remark 1: NF is defined according to source (input) resistance!

...which means that in cascaded systems, the output resistance of a preceding stage is needed to calculate the NF of the immediately next stage (more on this later).

- Remark 2: end-to-end voltage gain A (squared) is also needed!

Example 1:



$$V_{n,\text{out}}^2 = 4kT(R_S || R_P),$$

$$A_v = \frac{R_P}{R_S + R_P} \Rightarrow NF = 4kT(R_S || R_P) \frac{(R_S + R_P)^2}{R_P^2} \frac{1}{4kT R_S}$$
$$= 1 + \frac{R_S}{R_P}.$$

- Condition for minimum NF does not coincide with maximum power transfer.

Example 2 (Lossy circuit):

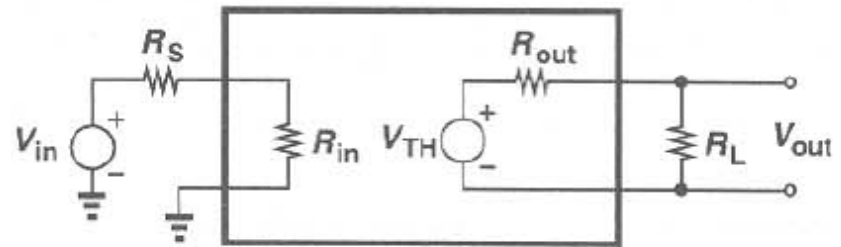
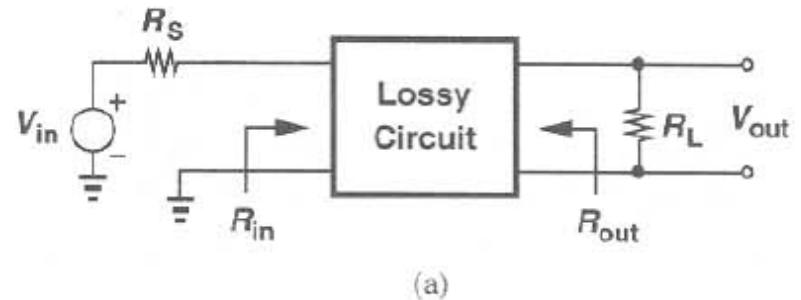
$$L = \frac{P_{in}}{P_{out}} \quad P_{in} \propto \frac{V_{in}^2}{R_s} \quad P_{out} \propto \frac{V_{TH}^2}{R_{out}}$$



$$L = \frac{V_{in}^2}{V_{TH}^2} \frac{R_{out}}{R_s}$$

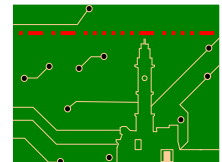
$$V_{n,out}^2 = 4kT R_{out} \frac{R_L^2}{(R_L + R_{out})^2}$$

$$A_v = \frac{V_{TH}}{V_{in}} \frac{R_L}{R_L + R_{out}}$$

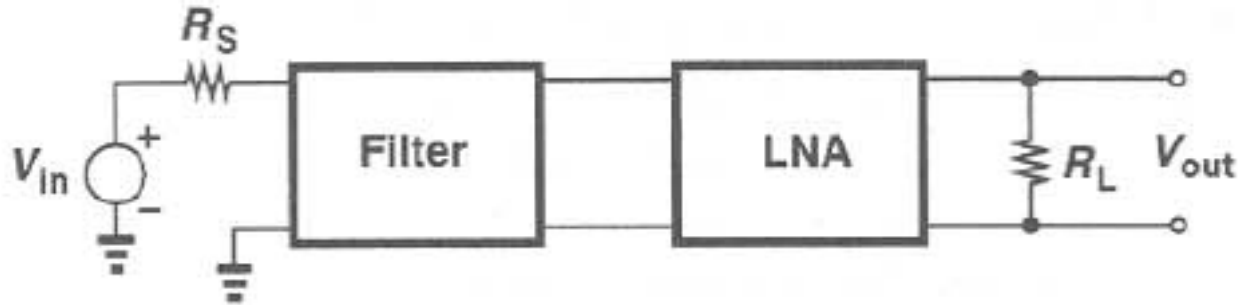
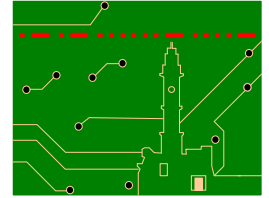


$$\Rightarrow NF = 4kT R_{out} \frac{V_{in}^2}{V_{TH}^2} \frac{1}{4kT R_s} = L.$$

- Power loss = NF for Lossy circuits (!!!)
- ATTENTION: L is power LOSS (not GAIN), i.e $L^{-1} = G$

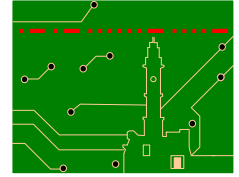


Example 3: series of Filter and LNA



$$\begin{aligned} NF_{\text{tot}} &= NF_{\text{filt}} + \frac{NF_{LNA} - 1}{L^{-1}} \\ &= L + (NF_{LNA} - 1)L \\ &= L \cdot NF_{LNA}, \end{aligned}$$

- **WARNING:** the above assumes that NF_{LNA} is referenced to input resistance equal to the output resistance of the above Filter...
- Usually in RF engineering, all systems are designed around 50 (75) Ω hm.
- Don't forget: Friss equation utilizes power gains (not voltage gains).



Notion of Sensitivity:

“the minimum signal level that the system can detect with acceptable signal-to-noise ratio”.

$$NF = \frac{SNR_{in}}{SNR_{out}} \Rightarrow P_{sig} = P_{RS} \cdot NF \cdot SNR_{out}$$

(Signal power per unit of BW)

$$= \frac{P_{sig}/P_{RS}}{SNR_{out}}$$

$$P_{sig,tot} = P_{RS} \cdot NF \cdot SNR_{out} \cdot B$$

$$P_{in,min}|_{dBm} = P_{RS}|_{dBm/Hz} + NF|_{dB} + SNR_{min}|_{dB} + 10\log B$$

$$P_{RS} = \frac{4kTR_S}{4} \frac{1}{R_{in}}$$

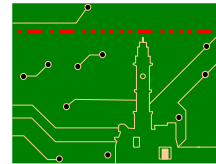
$$= kT$$

$$= -174 \text{ dBm/Hz}$$

Why 4?

÷ 2: rms value

÷ 2: power matching



Notion of Sensitivity:

“The minimum signal level that the system can detect with acceptable signal-to-noise ratio”.

$$P_{in,min}|_{dBm} = P_{RS}|_{dBm/Hz} + NF|_{dB} + SNR_{min}|_{dB} + 10\log B$$

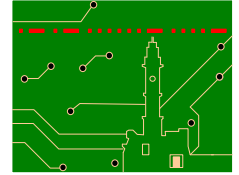


$$P_{in,min} = -174 \text{ dBm/Hz} + NF + 10\log B + SNR_{min}$$

=“noise floor F”

- WARNING1: small detectable signal (high sensitivity) might be the result of small communication bandwidth!
- WARNING2: SNR_{min} is the output, operational SNR.

Notion of Dynamic Range:

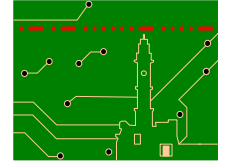


“The ratio of the maximum input level the system tolerates to the minimum signal level the system provides a reasonable signal quality”.

- notice that the definition is rather vague => different metric in ADCs, different metric in RF systems...
- RF systems: min signal according to sensitivity...
max signal according to intermodulation behavior,
i.e. input level where IM3 products equal noise floor.
=> “Spurious-free dynamic range (SFDR)”

$$P_{IIP3} = P_{in} + \frac{P_{out} - P_{IM,out}}{2}$$

Notion of Dynamic Range:



$$P_{IIP3} = P_{in} + \frac{P_{out} - P_{IM,out}}{2}$$



$$P_{IIP3} = P_{in} + \frac{P_{in} - P_{IM,in}}{2}$$

$$= \frac{3P_{in} - P_{IM,in}}{2},$$



$$P_{in} = \frac{2P_{IIP3} + P_{IM,in}}{3}$$



$$P_{in,max} = \frac{2P_{IIP3} + F}{3}$$

$$P_{out} - P_{IM,out} = P_{in} - P_{IM,in}$$

(remember geometric proof of IIP3!)

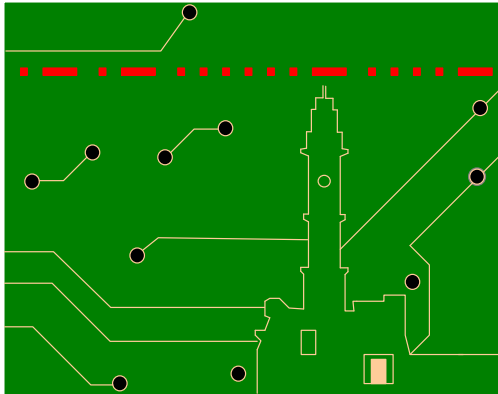
$$\begin{aligned} SFDR &= \frac{2P_{IIP3} + F}{3} - (F + SNR_{min}) \\ &= \frac{2(P_{IIP3} - F)}{3} - SNR_{min}. \end{aligned}$$

Example: IIP3=-15 dBm, NF=9 dB,
B=200kHz, SNR_{min}=12 dB

=> SFDR ≈ 53 dB

Think of the maximum relative level of interferer that a rec can tolerate for small desired input signal!

Questions?



Next lecture: Receiver Architectures!